Del Din S, Godfrey A, Rochester L. **Validation of an accelerometer to quantify a comprehensive battery of gait characteristics in healthy older adults and Parkinson’s disease: toward clinical and at home use.** *IEEE Journal of Biomedical and Health Informatics* 2015, (99).

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**DOI link to article:**

[http://dx.doi.org/10.1109/JBHI.2015.2419317](http://dx.doi.org/10.1109/JBHI.2015.2419317)

**Date deposited:**

02/06/2015
Validation of an accelerometer to quantify a comprehensive battery of gait characteristics in healthy older adults and Parkinson’s disease: toward clinical and at home use.

Silvia Del Din-IEEE Member, Alan Godfrey-IEEE Member and Lynn Rochester

Abstract—Measurement of gait is becoming important as a tool to identify disease and disease progression, yet to date its application is limited largely to specialist centres. Wearable devices enable gait to be measured in naturalistic environments however questions remain regarding validity. Previous research suggests that when compared with a laboratory reference, measurement accuracy is acceptable for mean but not variability or asymmetry gait characteristics. Some fundamental reasons for this have been presented (e.g. synchronisation, different sampling frequencies) but to date this has not been systematically examined. The aims of this study were to: (i) quantify a comprehensive range of gait characteristics measured using a single tri-axial accelerometer-based monitor, (ii) examine outcomes and monitor performance in measuring gait in older adults and those with Parkinson’s disease (PD) and (iii) carry out a detailed comparison with those derived from an instrumented walkway to account for any discrepancies. Fourteen gait characteristics were quantified in 30 people with incident PD and 30 healthy age-matched controls. Of the 14 gait characteristics compared, agreement between instruments was excellent for 4 (ICCs 0.913 – 0.983); moderate for 4 (ICCs 0.508 – 0.766); and poor for 6 characteristics (ICCs < 0.637 – 0.370). Further analysis revealed that differences reflect an increased sensitivity of accelerometry to detect motion, rather than measurement error. This is most likely because accelerometry measures gait as a continuous activity rather than discrete footfall events, per instrumented tools. The increased sensitivity shown for these characteristics will be of particular interest to researchers keen to interpret ‘real world’ gait data. In conclusion, use of a body worn monitor is recommended for the measurement of gait but is likely to yield more sensitive data for asymmetry and variability features.

Index Terms — Accelerometer, algorithm, body worn monitor, Instrumented gait, instrumented walkway.

I. INTRODUCTION

Gait is emerging as a powerful tool in neurodegenerative disease to identify surrogate markers of incipient disease manifestation or disease progression [1-5].

However, its widespread adoption for clinical and research purposes has been limited to date. This is largely because the majority of studies have been carried out using specialised gait analysis equipment (most commonly instrumented walkways such as pressure-sensor activated, e.g. GaitRite) [6-9] which limits work to specialised centres and a sparse number of gait cycles [10]. In order to develop the use of quantitative gait analysis for clinical screening and research, low-cost tools are required that facilitate measurement in the clinic and home. This has driven an interest in the use of accelerometer-based body worn monitors (BWM) for measuring gait.

BWM can provide a continuous sampling of whole body movement in controlled or habitual environments [11]. A BWM worn on the lower back implementing single/numerous algorithm(s) can provide a simple method to quantify gait; the adoption of the inverted pendulum model to evaluate step length and the use of appropriate filtering procedures to identify initial/ final contact events within the gait cycle [12-14]. However, it is essential to validate the combination of BWM and implemented algorithms to accurately capture gait outcomes before widespread adoption. Evidence suggests suitable validity and reliability of estimated mean values of gait outcomes to a trusted laboratory reference (GaitRite) [12, 13, 15-19]. Yet moderate to poor agreement has been reported for step-to-step fluctuations (variability) and bilateral coordination (asymmetry) [12, 14, 15, 17, 20-22]. This leaves the role of BWM to comprehensively quantify gait in ageing and pathology unclear.

A comprehensive examination of systems is lacking within the literature, which is critical to further understand and explain the poor agreement for asymmetry and variability gait characteristics. Previous studies have tried to provide a rationale for the poor agreement such as: difference in sampling rates; misalignment due to device orientation/placement; and poor synchronization [12, 13, 15, 23]. However, questions still remain. Furthermore, weaknesses of previous studies [12-15, 21] include: (i) limited and inconsistent reporting of gait characteristics [12-15]; (ii) introduction of newly derived variables [23-25] which are difficult to interpret making mainstream use problematic; (iii) restricted testing on a single (small) cohort (ranging on average from 10 to 23 participants [12, 13, 15, 20, 23]), often with a lack of consideration for the effects of pathology on BWM performance; and (iv) lack of BWM signal examination compared to video recordings. Evaluation of a comprehensive set of gait characteristics is therefore needed while undertaking a systematic examination of all data acquired during a validation-based study of a BWM.

The purpose of this study was therefore to take a systematic approach to address gaps in the literature. Firstly we aimed to characterise a broad range of gait characteristics using a low cost BWM in a large cohort of participants. Whilst multiple
characteristics can describe gait, studies have helped to provide a simplified framework for selection of important gait characteristics [5, 26, 27]. In this study characteristics were selected based on our previous work [27, 28] which identified a comprehensive range of 16 core gait characteristics (using GaitRite) recognised as indicative of healthy ageing and pathology (Parkinson’s disease, PD). Here, we used a BWM and adopted a novel combination of two algorithms to quantify gait grouped by the properties they measure such as summary mean values, variability and asymmetry and including phases of the gait cycle. Secondly, we wanted to compare results in PD and older adults to see if the performance of the BWM remained stable in pathology. The adoption of two cohorts is a key feature of this work, providing contrasting features of gait, where asymmetric and variability characteristics are known to differ. Finally, we compared the findings from the BWM to a common laboratory reference for comparability with previous work and where possible carried out a detailed evaluation where differences were found between systems in order to characterise the source of error. In adopting this process we wished to determine the ability of a low cost BWM to accurately measure a comprehensive set of core gait characteristics in normal and pathological conditions for confidence in more widespread adoption. This forms part of our ongoing work to quantify gait simply and effectively within laboratory-based instrumented testing sessions, with a view to quantifying gait in real world environments.

II. METHODS

A. Participants

Thirty PD patients within 4 months of diagnosis and 30 healthy aged matched control subjects (HC) were recruited from the Incidence of Cognitive Impairment in Cohorts with Longitudinal Evaluation—GAIT (ICICLE-GAIT) study. This is a collaborative study with ICICLE-PD, an incident cohort study (Incidence of Cognitive Impairment in Cohorts with Longitudinal Evaluation—Parkinson’s disease) conducted between June 2009 and December 2011 [29]. This study was conducted according to the declaration of Helsinki and had ethical approval from the Newcastle and North Tyneside research ethics committee. All participants signed an informed consent form prior to testing.

B. Demographic and Clinical Measures

Age, gender and body mass index (BMI) were recorded for each participant. Cognition was assessed with the Montreal Cognitive Assessment (MoCA) [30]. Balance confidence was measured using the self-rated Activities Balance Self Confidence Scale [31]. The severity of PD motor symptoms in the PD participants was measured using the Hoehn and Yahr scale [32], which ranges from 0 (no symptoms) to 5 (wheelchair bound or bedridden if unaided), and section III of the modified Movement Disorder Society version of the Unified Parkinson’s Disease Rating Scale (MDS-UPDRS [33]), which ranges from 0 (no motor symptoms) to 132 (severe motor symptoms). The Postural Instability and Gait Disorder (PIGD) and Tremor phenotype subscales were also calculated from the MDS-UPDRS [34]. Levodopa equivalent daily doses were calculated according to established methods [35].

C. Equipment

Each participant was asked to wear a low cost (<£100) tri-axial accelerometer-based device (Axivity AX3, dimensions: 23.0 × 32.5 × 7.6mm, weight: 9g) located on the fifth lumbar vertebrae (L5). Figure 1. It is a generic movement monitor that is non-specific for gait or ambulatory assessment and was held in place by double sided tape (Wig Tape, Natural Image, UK) and Hypafix (BSN Medical Limited, Hull, UK). The device measures vertical (a\(_v\)), anteroposterior (a\(_a\)) and mediolateral (a\(_m\)) accelerations and was programmed to capture data at 50Hz and 100Hz (16-bit resolution) and at a range of ±8g. The change in sampling frequency was due to upgrading of the device during the longitudinal ICICLE-PD Gait study where updated versions had increased memory and sampling capabilities. However, for consistency of analysis all data were down-sampled, where necessary, to 50 Hz.

Gait assessment was conducted concurrently as part of the ICICLE-GAIT study using a 7.0m long × 0.6m wide instrumented walkway (Platinum model GaitRite, software version 4.5, CIR systems, NJ, USA) which was synchronised with a video camera (Logitech, Webcam Pro 9000, CA, USA) recording at 25 Hz. The instrumented walkway had a spatial accuracy of 1.27cm and temporal accuracy of 1 sample (240Hz, ~4.17ms).

The quartz stabilised real time clock of the accelerometer (accuracy: 20 parts per million) was synchronised with the computer used for the walkway recordings and for each walking trial the start and stop time were recorded by the assessor. Start and stop times were subsequently input to a bespoke MATLAB® program that automatically segmented and analysed the accelerometer data. Digital synchronization to identify exact steps (left/right steps) between systems was not used due to the short distance traversed and lack of gyroscope within the BWM. However, the variability and asymmetry equations adopted in this study accounted for all steps to be used interchangeably (Section D. Laboratory reference: Instrumented walkway).

C. Protocol and Data Collection

Participants were asked to walk at their preferred speed, performing four intermittent straight line walking trials over 10.0m. The 7.0m instrumented walkway was placed in the centre of the 10.0m (Figure 1) to ensure gait was captured at a steady speed. In addition synchronised video of frontal plane motion was recorded during each walk. PD participants who were on medication were tested approximately 1 hour after medication intake.

Figure 1. The tri-axial accelerometer-based device and site of attachment on the lower back (L5) and laboratory set up for testing intermittent walks.
D. Data Analysis
BWM (accelerometer) data processing

The BWM data were downloaded to a computer, segmented into the 4 different straight line passes using time stamps and analysed by the MATLAB® program. Accelerometer signals were transformed to a horizontal-vertical coordinate system [36], and filtered with a 4th order Butterworth filter at 20 Hz [12, 14] using the MATLAB functions: detrend, butter, and filtfilt. For the purposes of this study the program utilised the novel application of a combination of gait algorithms that have been previously developed for a single sensor attached to L5 on a cohort of healthy older adults:

Gait algorithm #1

The first algorithm estimated the initial contact (IC) and final contact (FC) events within the gait cycle (Figure 2), and is described in detail elsewhere [12]. In brief the algorithm consisted of the following:

- The IC and FC events are estimated from a continuous wavelet transform (CWT, using the cwt MATLAB® function) of $a_i$, which was first integrated (cumtrapz) and then differentiated using a Gaussian CWT: the IC events were detected as the local minima of the CWT (findpeaks). Figure 3a. A further differentiation resulted in the local maxima being defined as the FC events (Figure 3a, Figure 4).

Previously, the algorithm has been used to estimate step and stride times only [12]. However, in order to fully replicate the core characteristics of gait we needed to derive stance and swing time. This was achieved through the sequence of IC and FC events in relation to the double support phase of the gait cycle, Figure 2. From the sequence (i) of IC and FC events both left and right (opposite) events were identified where stride and subsequently stance and swing time were estimated, Equations (1, 2 & 3). For direct comparison to the steps quantified by the instrumented walkway, the initial and final 4 steps (walk to/from the walkway) of the accelerometer data (as determined by the IC/FC algorithm) were excluded from analysis.

Gait algorithm #2

Upon initial inspection of the signal traces, spurious IC events (i.e. non-IC events, Figure 4a) were detected in 37% and 58% of the HC and PD groups, respectively. As a result, the algorithm to detect IC and FC events was refined to include a previous methodology for improved step detection: the updated algorithm only included IC peaks within a predetermined time lapse similar to Najafi et al. [17]. The optimisation procedure required IC events to be identified during a predefined interval (0.25-2.25s) from a previous IC event. Figure 4b shows an example of the updated algorithm with the correct estimation of IC and FC events.

Figure 2. Identification of stride, stance and swing times from the double support phase of the IC and FC algorithm

Stance time = FC$(i + 1) − IC(i)$  \hspace{1cm} (1)
Stride time = IC$(i + 2) − IC(i)$  \hspace{1cm} (2)
Swing time = Stride time − Stance time  \hspace{1cm} (3)

Gait algorithm #3

To estimate a value for step velocity we utilised algorithm #1 and #2 and the simple ratio between distance (length) and time, Equation 5.

Step Velocity = Step Length/Step Time  \hspace{1cm} (5)
Laboratory reference: Instrumented walkway

Data for individual steps for each walk were extracted from the instrumented walkway database using Microsoft Access 2007 (Microsoft Corp., Redmond, WA, USA). Mean gait values were calculated for step time, stance time (duration the stance foot was in contact with the ground for a given stride), swing time (duration a foot was not in contact with the ground for a given stride), step length and step velocity. To calculate step variability, the standard deviation (SD) from all steps (left and right combined) was calculated, Equation 6. SD was selected as a measure of variability due to its robustness and dual use with both the BWM and walkway. Other measures of variability (harmonic ratio, coefficient of variation) have been suggested but have shown low to moderate agreement between systems [23, 24, 38, 39] and are not all quantifiable by an instrumented walkway.

Equation 6. SD was selected as a measure of variability due to its robustness and dual use with both the BWM and walkway. Other measures of variability (harmonic ratio, coefficient of variation) have been suggested but have shown low to moderate agreement between systems [23, 24, 38, 39] and are not all quantifiable by an instrumented walkway.

III. RESULTS

Demographic data

Participant demographic, clinical and cognitive descriptors are shown in Table I. Compared to HC, PD participants were aged matched; included proportionally less women (CL: 50%, PD: 33%); presented with lower confidence in their balance (ABCs), and poorer cognition (MoCA). No differences were found between HC and PD participants for both height and BMI. Participants with PD were in the early stages of the disease with mild motor symptoms.

BWM and Instrumented walkway: agreement

Table II shows the agreement between the two systems for ICC, r values and LoA (%). There was excellent agreement between the systems for all the mean gait variables (step velocity, step time, stance time and step length) except for swing time. In contrast asymmetry of steps (bilateral co-ordination) and variability (step to step fluctuations) showed poor agreement.

Table III shows the results obtained from the derived gait parameters for both the BWM and instrumented walkway. Results show that the BWM had systematic longer/greater gait characteristics and this is significant for 10 of the 14 and 9 of the 14 variables for HC and PD, respectively.
TABLE I. CLINICAL AND DEMOGRAPHIC CHARACTERISTICS

<table>
<thead>
<tr>
<th>Characteristic</th>
<th>HC (n = 30) Mean ± SD</th>
<th>PD (n = 30) Mean ± SD</th>
<th>p</th>
</tr>
</thead>
<tbody>
<tr>
<td>M/F (n)</td>
<td>15/15</td>
<td>20/10</td>
<td>0.197</td>
</tr>
<tr>
<td>Age (years)</td>
<td>66.6 ± 7.7</td>
<td>66.9 ± 9.4</td>
<td>0.891</td>
</tr>
<tr>
<td>Height (m)</td>
<td>1.7 ± 0.1</td>
<td>1.7 ± 0.1</td>
<td>0.795</td>
</tr>
<tr>
<td>BMI (Kg/m²)</td>
<td>28.0 ± 4.6</td>
<td>28.7 ± 5.4</td>
<td>0.585</td>
</tr>
<tr>
<td>MoCA (0-30)</td>
<td>27.9 ± 1.7</td>
<td>24.7 ± 3.1</td>
<td>&lt;0.001</td>
</tr>
<tr>
<td>ABCs (0-100%)</td>
<td>91.3 ± 12.7</td>
<td>81.7 ± 20.0</td>
<td>0.031</td>
</tr>
<tr>
<td>Hoehn &amp; Yahr (n)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>HY I - 8</td>
<td>HY II - 20</td>
<td></td>
</tr>
<tr>
<td>Levodopa Equivalent</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Daily Dose (mg/day)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>MDS-UPDRS III</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Motor Phenotype (n)</td>
<td></td>
<td></td>
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</tr>
</tbody>
</table>

BWM and Instrumented walkway: examination #1

To explore differences between systems for variability and asymmetry an analysis was conducted to check the potential impact of the quality of the measured filtered acceleration aₜ on the differences observed. For exploratory purposes we decided to examine step time variability obtained by both systems.

A range of features based on the filtered aₜ were calculated and averaged across the 4 passes: mean, standard deviation, root mean square values (RMS), number of peaks (maxima of aₜ) and valleys (minima of aₜ), number of zero crossing (ZC), and frequency below which is the 95% of the signal power spectrum (95%). Pearson’s correlations explored the association between each of these features and the differences in step time variability of the two systems. None of the extracted features showed a strong positive correlation in either group (r < 0.353, Table IV), demonstrating that the poor agreement for the variability results could not be explained by the nature of the acceleration signal.

TABLE II. AGREEMENT BETWEEN INSTRUMENTED WALKWAY AND BWM

<table>
<thead>
<tr>
<th>Variable</th>
<th>HC</th>
<th>PD</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>ICC₂₁, r</td>
<td>LoA</td>
</tr>
<tr>
<td>Step time (s)</td>
<td>0.983, 0.998</td>
<td>1.2</td>
</tr>
<tr>
<td>Stance time (s)</td>
<td>0.927, 0.912</td>
<td>9.5</td>
</tr>
<tr>
<td>Swing time (s)</td>
<td>0.766, 0.708</td>
<td>18.0</td>
</tr>
<tr>
<td>Step length (m)</td>
<td>0.913, 0.867</td>
<td>13.9</td>
</tr>
<tr>
<td>Step vel. (m/s)</td>
<td>0.952, 0.906</td>
<td>14.7</td>
</tr>
<tr>
<td>Variability (var) gait characteristics</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Step time var (s)</td>
<td>0.508, 0.429</td>
<td>100.9</td>
</tr>
<tr>
<td>Stance time var (s)</td>
<td>0.645, 0.747</td>
<td>159.9</td>
</tr>
<tr>
<td>Swing time var (s)</td>
<td>0.307, 0.302</td>
<td>206.7</td>
</tr>
<tr>
<td>Step length var (m)</td>
<td>0.060, 0.102</td>
<td>126.3</td>
</tr>
<tr>
<td>Step vel. var (m/s)</td>
<td>-0.143, -0.086</td>
<td>110.2</td>
</tr>
<tr>
<td>Asymmetry (asy) gait characteristics</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Step time asym (s)</td>
<td>-0.637, -0.349</td>
<td>268.2</td>
</tr>
<tr>
<td>Stance time asym (s)</td>
<td>0.370, 0.249</td>
<td>177.2</td>
</tr>
<tr>
<td>Swing time asym (s)</td>
<td>-0.229, -0.111</td>
<td>316.1</td>
</tr>
<tr>
<td>Step length asym (m)</td>
<td>0.132, 0.078</td>
<td>243.5</td>
</tr>
</tbody>
</table>

Figure 5. Step time and step time variability (SD) evaluated with the instrumented walkway and the BWM for HC and PD participant. The BWM show higher step time variability for both (a) HC and (b) PD.
TABLE III. MEAN ± SD VALUES AND MEAN DIFFERENCES OF 14 GAIT PARAMETERS EVALUATED WITH AN INSTRUMENTED WALKWAY AND BWM

<table>
<thead>
<tr>
<th>Characteristic</th>
<th>Instrumented walkway</th>
<th>BWM</th>
<th>Mean Difference, %</th>
<th>Instrumented walkway</th>
<th>BWM</th>
<th>Mean Difference, %</th>
<th>P</th>
</tr>
</thead>
<tbody>
<tr>
<td>Step time (s)</td>
<td>0.554 ± 0.051</td>
<td>0.567 ± 0.054</td>
<td>0.013, 2.4%</td>
<td>0.543 ± 0.045</td>
<td>0.555 ± 0.047</td>
<td>0.012, 2.2%</td>
<td>&lt;0.001</td>
</tr>
<tr>
<td>Stance time (s)</td>
<td>0.715 ± 0.080</td>
<td>0.731 ± 0.062</td>
<td>0.016, 2.2%</td>
<td>0.706 ± 0.072</td>
<td>0.717 ± 0.063</td>
<td>0.011, 1.6%</td>
<td>0.119</td>
</tr>
<tr>
<td>Swing time (s)</td>
<td>0.393 ± 0.031</td>
<td>0.404 ± 0.051</td>
<td>0.011, 2.7%</td>
<td>0.380 ± 0.029</td>
<td>0.394 ± 0.044</td>
<td>0.014, 3.7%</td>
<td>0.052</td>
</tr>
<tr>
<td>Step length (m)</td>
<td>0.692 ± 0.094</td>
<td>0.718 ± 0.099</td>
<td>0.026, 3.7%</td>
<td>0.638 ± 0.100</td>
<td>0.681 ± 0.089</td>
<td>0.043, 6.7%</td>
<td>&lt;0.001</td>
</tr>
<tr>
<td>Step vel. (m/s)</td>
<td>1.266 ± 0.219</td>
<td>1.275 ± 0.220</td>
<td>0.009, 0.7%</td>
<td>1.187 ± 0.223</td>
<td>1.242 ± 0.218</td>
<td>0.055, 4.6%</td>
<td>&lt;0.001</td>
</tr>
</tbody>
</table>

Variability (var) gait characteristics

<table>
<thead>
<tr>
<th>Characteristic</th>
<th>Instrumented walkway</th>
<th>BWM</th>
<th>Mean Difference, %</th>
<th>Instrumented walkway</th>
<th>BWM</th>
<th>Mean Difference, %</th>
<th>P</th>
</tr>
</thead>
<tbody>
<tr>
<td>Step time var (s)</td>
<td>0.017 ± 0.008</td>
<td>0.024 ± 0.011</td>
<td>0.007, 32.8%</td>
<td>0.022 ± 0.012</td>
<td>0.031 ± 0.023</td>
<td>0.009, 41.8%</td>
<td>0.099</td>
</tr>
<tr>
<td>Stance time var (s)</td>
<td>0.022 ± 0.012</td>
<td>0.026 ± 0.015</td>
<td>0.005, 21.8%</td>
<td>0.023 ± 0.010</td>
<td>0.033 ± 0.022</td>
<td>0.011, 46.3%</td>
<td>0.003</td>
</tr>
<tr>
<td>Swing time var (s)</td>
<td>0.016 ± 0.009</td>
<td>0.027 ± 0.024</td>
<td>0.011, 66.3%</td>
<td>0.019 ± 0.007</td>
<td>0.031 ± 0.025</td>
<td>0.013, 65.9%</td>
<td>0.004</td>
</tr>
<tr>
<td>Step length var (m)</td>
<td>0.023 ± 0.007</td>
<td>0.043 ± 0.021</td>
<td>0.021, 92.6%</td>
<td>0.025 ± 0.008</td>
<td>0.040 ± 0.015</td>
<td>0.015, 57.6%</td>
<td>&lt;0.001</td>
</tr>
<tr>
<td>Step vel. var (m/s)</td>
<td>0.058 ± 0.017</td>
<td>0.043 ± 0.021</td>
<td>-0.015, 25.4%</td>
<td>0.062 ± 0.023</td>
<td>0.040 ± 0.015</td>
<td>-0.022, 35.8%</td>
<td>&lt;0.001</td>
</tr>
</tbody>
</table>

Asymmetry (asy) gait characteristics

<table>
<thead>
<tr>
<th>Characteristic</th>
<th>Instrumented walkway</th>
<th>BWM</th>
<th>Mean Difference, %</th>
<th>Instrumented walkway</th>
<th>BWM</th>
<th>Mean Difference, %</th>
<th>P</th>
</tr>
</thead>
<tbody>
<tr>
<td>Step time asy (s)</td>
<td>0.010 ± 0.006</td>
<td>0.015 ± 0.014</td>
<td>0.005, 38.2%</td>
<td>0.023 ± 0.027</td>
<td>0.023 ± 0.044</td>
<td>-0.0001, 0.3%</td>
<td>0.990</td>
</tr>
<tr>
<td>Stance time asy (s)</td>
<td>0.020 ± 0.012</td>
<td>0.014 ± 0.013</td>
<td>-0.006, 30.9%</td>
<td>0.022 ± 0.009</td>
<td>0.023 ± 0.045</td>
<td>0.001, 6.9%</td>
<td>0.846</td>
</tr>
<tr>
<td>Swing time asy (s)</td>
<td>0.010 ± 0.010</td>
<td>0.013 ± 0.015</td>
<td>0.003, 29.7%</td>
<td>0.018 ± 0.016</td>
<td>0.019 ± 0.024</td>
<td>0.001, 4.8%</td>
<td>0.848</td>
</tr>
<tr>
<td>Step length asy (m)</td>
<td>0.022 ± 0.016</td>
<td>0.014 ± 0.017</td>
<td>-0.008, 37.8%</td>
<td>0.024 ± 0.017</td>
<td>0.014 ± 0.015</td>
<td>-0.010, 4.6%</td>
<td>0.023</td>
</tr>
</tbody>
</table>

Mean difference: BWM – Instrumented walkway; Step vel.: Step velocity.

TABLE IV: RESULTS BETWEEN α, FEATURES AND DIFFERENCES BETWEEN INSTRUMENTED WALKWAY AND BWM STEP VARIABILITY

<table>
<thead>
<tr>
<th>Features</th>
<th>HC</th>
<th>PD</th>
</tr>
</thead>
<tbody>
<tr>
<td>Mean ± SD</td>
<td>r</td>
<td>Mean ± SD</td>
</tr>
<tr>
<td>Mean a_i</td>
<td>-0.990 ± 0.067</td>
<td>0.094</td>
</tr>
<tr>
<td>SD a_i</td>
<td>0.127 ± 0.050</td>
<td>0.353</td>
</tr>
<tr>
<td>RMS a_i</td>
<td>1.006 ± 0.067</td>
<td>0.003</td>
</tr>
<tr>
<td># of peaks</td>
<td>128 ± 42</td>
<td>0.095</td>
</tr>
<tr>
<td># of valleys</td>
<td>108 ± 29</td>
<td>&lt;0.001</td>
</tr>
<tr>
<td>ZCR</td>
<td>131 ± 37</td>
<td>0.009</td>
</tr>
<tr>
<td>95%</td>
<td>10.660 ± 2.372</td>
<td>0.108</td>
</tr>
</tbody>
</table>

RMS: Root Mean Square values; SD: Standard Deviations; #: number; ZCR: Zero crossing; 95%: frequency below which is the 95% of the signal power spectrum

i) Where gait was clearly asymmetrical (e.g. PD), asymmetry results were comparable (Figure 6a), while more subtle asymmetric gait patterns (e.g. HC) were detected by the BWM but not instrumented walkway (Figure 6b). This may explain the higher agreement for PD participants’ asymmetry results compared to HC (step time asymmetry, Table II and Table III: people with PD often show a clear asymmetric gait pattern, whilst asymmetry is not as pronounced a feature in HC. This was confirmed in individual patient videos which were used as a reference to identify subtle features of gait identified by expert physiotherapists and biomechanists.

ii) Where gait was clearly asymmetrical (e.g. PD), asymmetry results were comparable (Figure 6a), while more subtle asymmetric gait patterns (e.g. HC) were detected by the BWM but not instrumented walkway (Figure 6b). This may explain the higher agreement for PD participants’ asymmetry results compared to HC (step time asymmetry, Table II and Table III: people with PD often show a clear asymmetric gait pattern, whilst asymmetry is not as pronounced a feature in HC. This was confirmed in individual patient videos which were used as a reference to identify subtle features of gait identified by expert physiotherapists and biomechanists.

IV. DISCUSSION

This study replicated 14 core characteristics of gait from a generic tri-axial accelerometer-based movement monitor using a novel combination of gait algorithms (BWM) to segment the gait cycle into discrete events. It is the largest and most comprehensive evaluation to date which incorporates comparison of pathological and non-pathological cohorts.

We compared the BWM results to a known laboratory reference (instrumented walkway, GaitRite) and were able to explain the systematic differences between systems unresolved by previous research.

Mean characteristics and effect of pathology

Excellent (ICCs > 0.900, LoA < 15.0%) agreement was found for mean step time, stance time, step length, and step velocity for HC (ICCs_{2,1} ≥ 0.913) and for step time, stance time, and step velocity for PD (ICCs ≥ 0.913), similar to other studies [12, 15]. Good agreement (ICCs 0.751 – 0.899, LoA > 15.0%) was found for swing time for HC (ICC_{2,1} = 0.766) and step length for PD (ICC_{2,1} = 0.869) similar to previous findings [15]. In contrast we only found moderate agreement (ICCs 0.500 – 0.750) for swing time for PD (ICCs = 0.511).

The poorer agreement for mean swing time could be related to the limitation of the FC/IC algorithm where swing time was not accounted for in its design. Though the
algorithm [12] evaluated IC and FC events, the authors presented step and stride time values, which is based on IC estimation only. However, the detection of FCs allowed us to derive stance and swing time with contrasting results for both. Moreover, error is inherently assumed as swing time was computed in our study from the difference between stride and stance time, where small inaccuracies may also exist. Swing time estimation may be improved from direct IC and FC analysis rather than the method adopted here based on the relationship between stance, swing and stride time within the gait cycle.

Good agreement was found for step length within the PD group while the HC had excellent agreement (ICC$_{2,1}$ = 0.913), similar to another study [15]. LoA for HC and PD were < 16.0% and mean percentage difference 3.7% for HC and 6.7% for PD which equates to longer estimated distances of 0.026m and 0.043m, respectively, which we consider acceptable [15]. Traditionally, high reproducibility has been problematic with step length due to adoption of the inverted pendulum model on which it is based [14, 40, 41]. The model assumes a compass gait cycle (circular trajectory) [14], which is not the case in an asymmetric disease (PD). Moreover, the model also assumes straight line walking at a constant pace which makes it problematic when testing within pathology or during laboratory-based protocols where continuous walking for better gait variability estimation is the recommendation [42]. Thus, there is a need to better refine step length estimation where the calculation of vertical displacement (h), pendulum length (l) or the adoption of a generic correction factor are sources of error.

Algorithms independent of site specific variables (h, l) and correction factors will allow for more robust quantification of step length. To date individualised correction factors have been recommended for improved step length estimation rather than generic or group specific values [18, 20]. However, these would be time consuming and difficult to implement in day-to-day clinical practice or in large scale clinical/intervention-based studies where instrumentation of gait is often time constraint [43]. We were unable to calculate estimates for the remaining core gait characteristics, i.e. step width and step width variability due to the limitations of the BWM and adoption of a single tri-axial accelerometer. Moreover, step width estimation is yet to be determined from a single accelerometer-based BWM due to the bipedal dynamics of human locomotion and relative mediolateral placement of feet.

**Variability and asymmetry characteristics and effect of pathology**

We found poor to moderate agreement between systems for all variability and asymmetry characteristics, similar to previous studies [23, 24, 38, 39, 44]. Therefore we conducted an analysis to explore the lack of agreement to offer new insight into gait quantification with these systems. We hypothesised that corrupt features of the filtered acceleration signal would impact on the error between systems. However, there were no significant correlations in any of the extracted features, verifying that the standard filtering procedure (4th order Butterworth, cut off 20Hz) and resulting signal were robust. Further exploration of the all the filtered acceleration signals together with all participant videos highlighted subtle asymmetries in gait that were only evident in the BWM signal and not instrumented walkway. A number of possible explanations account for these differences:

i) We found that height of the participants had an impact on the error of the estimation of stance time asymmetry and swing time variability and this can be related to the limitation of the FC/IC algorithm. Asymmetry was more comparable between instruments for PD because it is a more prominent feature of pathological gait. Asymmetry in HC is subtle and more difficult to detect with an instrumented walkway due to slight variations in dynamics of the CoM rather than discrete footfalls. These results impact on variability which was not comparable. Greater asymmetry increases the estimation of variability for accelerometry given its sensitivity to detecting this feature of gait.

ii) An instrumented walkway detects footfalls but an accelerometer-based BWM continuously tracks the position of the body resulting in a continuous signal (Figure 4 and 6). The resulting peak therefore represents the trajectory of the CoM rather than actually heel strike (IC) or toe off (FC) events determined by an instrumented walkway.

iii) Gait algorithms are dependent on the signal characteristics (e.g. peaks reliant on polynomial coefficients or local maxima to locate the maximum of a peak). Thus, delay in the location of the maximum/minimum due to peak detection methods or smoothness of peak as a result of filtering or processing can introduce timing differences between the BWM signal and instrumented walkway to a resolution required for variability/asymmetric outcomes (ms).

**Instrumented walkway: functionality and sources of error**

The instrumented walkway used in this study (GaitRite) has been previously shown to be a reliable method for measuring mean gait characteristics [45], but less so for asymmetry and variability [23, 24, 38, 39]. Another plausible explanation for these discrepancies is the operational functionality of the walkway itself. Specifically the walkway is an array of pressure sensors that activate or trigger a footfall event when a load is applied. These events usually occur as a collective to define the entire surface area of the foot and subsequently IC and FC events. However, spurious contacts may result due to scuffing or a shuffling walk introducing false IC events. As a result, the technician/researcher can review the series of contacts (activated pressure sensors) for each footfall and subjectively include or exclude an individual sensor (within the array defining a foot) if they deem it suitable during a walk. With a spatial accuracy of 1.27cm this (subjective) inclusion/exclusion of sensors can be the difference of approximately 0.009s based on an estimated stepping speed (step velocity 142cm/s). With variability and asymmetry quantified at a similar resolution (Table III), the inclusion/exclusion of a single pressure sensor in the
walkway can be a further source of disagreement between systems.

**Alternative laboratory reference**

Previous work has used continuous tracking of the CoM with a 3D motion analysis system [21, 46, 47]. Direct comparison of vertical acceleration, velocity, and position (displacement) traces together with spatial-temporal parameters showed good agreement between the optical motion capture system and an inertial measurement unit (BWM) [21, 46]. Despite good agreement, the comparison of an accelerometer-based BWM to a 3D system, though more similar in quantification of gait, measure different components; acceleration and displacement, respectively. Though acceleration and displacement can be related through single and double integration/derivation, that process introduces error through drift, where the error in the signal after each integration increases by $\epsilon = \epsilon^t$, where $t$ is integration time and $\epsilon$ is error [21, 48].

Therefore systematic errors will always remain between systems (instrumented walkway vs. accelerometer-based BWM on the lower back (L5) vs. 3D motion analysis system) even when measuring related components explaining why in our study there is lower agreement for the mean swing time, higher variability of step time (Figure 6) and estimation of (subtle) symmetry differences. This however does not infer that one system is less valid, rather that both systems are valid but differences can be explained by different methodological approaches used to estimate gait events.

BWM tend to have greater estimates for gait characteristics (a feature of the adopted algorithms), but was systematic in its nature and the values remained within expected ranges for both PD and HC. Importantly, pathology did not influence our findings although this may change with increased disease severity and gait impairment.

**Study limitations and future work**

This study achieved its aims of quantifying 14 core gait characteristics while also deriving a new rationale to account for poor agreement between a BWM (worn at L5) and an instrumented walkway. However, some limitations do exist and therefore we make recommendations for future research. For instance, the methodology presented has been tested in a laboratory environment, considering walking at self-selected speed on a group of healthy participants and those with PD. Therefore before being able to generalize our results in these groups, further analysis would be required to test the robustness of the combination of algorithms across different gait speeds.

Moreover, our PD group had mild motor symptoms and more severe motor symptoms may influence the gait pattern and algorithm performance. For instance, lack of clearly identifiable signal characteristics (peaks/troughs) within the filtered signal may result in the miss or no detection of IC/FC events. While we included a range of PD participants (PIGD, ID, TD) there was no major (visually observant) limitation within their gait such as shuffling.

The addition of a gyroscope sensor within the BWM would allow the complete quantification of the 16 gait characteristics identified as important [27, 28]. Additionally, the extra sensor would allow the correct identification and allocation of left/right steps. The improved step recognition methodology would allow the variance of left and right steps to be calculated separately and then be combined to find SD, Equation 8. This method
avoids confounding step-to-step variability with variation originating from asymmetry between left and right steps [42]. Moreover, the correct identification of each left/right step could then be directly compared between systems

\[
SD_{\text{left or right}} = \sqrt{\frac{(\text{Variance}_{\text{left}} + \text{Variance}_{\text{right}})}{2}} \tag{8}
\]

V. CONCLUSION

A simple tri-axial accelerometer device is able to replicate 14 clinically relevant core gait characteristics. Agreement with a laboratory reference system ranged from excellent (mean) to poor (variability and asymmetry), which we interpreted as primarily an intrinsic limitation of the comparison between two systems which measure different properties: continuous motion (BWM) vs. single football events (instrumented walkway). Despite this, we feel confident from our results that a single tri-axial accelerometer-based BWM is accurate for measuring gait variability and asymmetry.

Accelerometer-based BWM may offer advantages over standard laboratory systems for select characteristics potentially making them a more sensitive device to detect any subtle changes in gait pattern due to ageing and/or pathology. When compared to an instrumented walkway, systematically greater values of mean gait characteristics need to be taken into consideration. However, a system currently doesn’t exist which: captures a broad range of gait outcomes sensitive to early pathology, is low-cost (<£100), and capable of being deployed in multi-centre large scale studies for instrumented testing or within the community for real-world continuous data collection. This approach (use of a generic movement monitor and algorithms from the literature) may therefore offer a low-cost solution for quantitative gait evaluation in PD and HC during instrumented testing and in a wide variety of environments (including at home). Further work is ongoing to optimise gait quantification algorithms as well as explore step width estimation and the impact of algorithm sensitivity on disease progression and disease severity.

ACKNOWLEDGMENT

We would like to acknowledge Dr. Brook Galna for his assistance in data analysis and interpretation and Dr. Sue Lord for critical examination of the manuscript.

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This article has been accepted for publication in a future issue of this journal, but has not been fully edited. Content may change prior to final publication. Citation information: DOI 10.1109/JBHI.2015.2419317, IEEE Journal of Biomedical and Health Informatics